NorCal Engineering

Soils and Geotechnical Consultants 10641 Humbolt Street Los Alamitos, CA 90720 (562) 799-9469 Fax (562) 799-9459 OCT 3 1 2005

October 27, 2005

Project Number 11233-04 Permit No. 04030-10000-02507

Boeing Realty Corp 15480 Laguna Canyon Road #200 Irvine, California 92618

RE: Final Geotechnical Report - Observation and Testing for Proposed Office/Warehouse Project – Located at 1451 West Knox Street, in the City of Los Angeles, California (Lot 8, Tract 52172)

Dear Sirs:

Pursuant to your request, this firm has provided this geotechnical report to summarize the observation and testing performed during grading operations at the above referenced project. The geotechnical aspects of the rough grading were conducted in accordance with our report titled "Geotechnical Investigation" dated March 13, 2004, Project Number 11233-04. Our geotechnical services pertaining to the grading of the project development are summarized in the subsequent sections of this report.

Previous Site Work

The property was previously graded between February, 2001 and May, 2002 during mass grading of the area. All existing fill soils on the subject lots were removed to competent native soils and the bottom observed and approved by a representative of this firm prior to replacement of compacted fill soils. Approximately 10 to 30 feet of fill was placed on site, although local variations in the excavation bottom could cause the actual fill depth to vary slightly.

No subsurface obstructions were abandoned in place on the subject lots during grading operations. The report dated in 2002, by NorCal Engineering details the rough grading of the property. A copy of the approval letter for our compaction report and the soils report approval letter are included in Appendix C.

The fill placed was certified as a "secondary fill", suitable for placement of slabs-on-grade and pavement. The referenced geotechnical investigation and testing was performed in order to reclassify the fill as "primary", suitable for placement of structural foundations as well as slabs-on-grde and pavement.

Site Grading

The purpose of the grading operations was for the placement of fill to provide primary support (building pad, foundation and pavement areas) of the proposed development. All vegetation and demolition debris was stripped and removed from the fill area prior to the placement of any fill soils. The upper low density surface soils (upper 12 to 18 inches) were removed to competent engineered fill and the bottom approved by a representative of this firm prior to placement of compacted fill soils. The exposed surface was scarified, moisture conditioned and then recompacted to a minimum of 90% relative compaction. Excavated soils were reutilized as compacted fill once any deleterious or oversized material (in excess of eight inches) was removed.

Foundation areas are underlain by a sufficient thickness of engineered fill to provide a minimum three feet thick compacted fill blanket beneath foundations. In the opinion of this firm, the engineered fill soils are suitable to support the placement of fill material. Grading extended a minimum of five horizontal feet or to the depth of fill placed, whichever is greater, beyond the edge of the proposed foundations.

Fill soils placed were compacted to a minimum 90% of the laboratory standard in lifts not in excess of eight inches in thickness. Areas that tested below 90% compaction were reworked and retested until a minimum of 90% relative compaction and near optimum moisture levels could be achieved. The maximum depth of fill soils placed was approximately 5 feet in the building pad area. The upper one foot of the building pad was compacted to a minimum of 95% of the laboratory standard.

No import soils were used during recent grading operations. The soil bearing capacity of the compacted fill on-site was established using shear test data included in our March, 2004 report. A copy of the shear test results is attached in Appendix A.

Conventional earthmoving equipment was utilized for compaction control. A water truck provided moisture control. Our services did not include any surveying of excavation bottoms, building corners, or subgrade elevations during grading operations.

Laboratory/Field Testing

The relative compaction was determined by Sand Cone Method (ASTM: D1556-00). The maximum density of the fill soils was obtained by the laboratory standard (ASTM: D1557-00) and results are shown on Table I. Tests were performed a minimum of every 500 cubic yards placed and every two feet in depth of fill placed. A summary of the compaction tests are described in Appendix B with locations shown on the accompanying plan. Additional laboratory tests were performed on representative bulk bag samples of the near surface soils at the completion of precise grading operations. The tests consisted of the following:

- A. Expansion index tests in accordance with the Uniform Building Code Standard No. 18-2 were performed on remolded samples of the upper soils to determine the expansive characteristics and to provide any necessary recommendations for reinforcement of the slabs-on-grade and the foundations. Results of these tests are provided on Table II in Appendix A.
- B. Soluble sulfate tests in accordance with California Test Method 417 were performed on representative soils samples to estimate the potential for corrosion of concrete in contact with the on-site soils. Results are provided on Table III in Appendix A.
- C. Direct shear tests (ASTM: D-3080) were performed on undisturbed and disturbed samples of the subsurface soils. The test is performed under saturated conditions at loads of 500 lbs./sq.ft., 1,000 lbs./sq.ft., and 2,000 lbs./sq.ft. with results provided on Table IV in Appendix A.

Foundation Design

All foundations may be designed utilizing the following allowable soil bearing capacities for an embedded depth of 24 inches into stiff compacted fill materials with the corresponding widths:

Allowable Soil Bearing Capacity (psf)

| | Continuous | Isolated |
|------------|------------|-------------------|
| Width (ft) | Foundation | <u>Foundation</u> |
| 1.5 | 2000 | 2500 |
| 2.0 | 2050 | 2550 |
| 4.0 | 2250 | 2750 |
| 6.0 | 2450 | 2950 |

A substantial decrease in the above bearing capacities will be necessary if the required compacted fill blanket is not provided beneath and outside of foundations. A one-third increase may be used when considering short term loading from wind and seismic forces. Foundations located at property line shall utilize a reduced allowable soil bearing capacity of 1,500 psf. Foundations shall be embedded a minimum of 24 inches below lowest adjacent soil grade and into stiff compacted fill soils as verified by the soil engineer.

All continuous foundations shall be reinforced with a minimum of four, #4 bars, two top and bottom. Isolated foundations may be reinforced at the discretion of the project structural engineer. In addition, foundation excavations observed and approved by a representative of this firm prior to pouring concrete were embedded into competent bearing material.

Slab Design

All concrete slabs-on-grade in warehouse and office areas shall be at least 6 and 5 inches in thickness, respectively, and may be placed on fill soils compacted to a minimum of 95% relative compaction in the upper 12 inches. Soils below the upper 12 inches may be compacted to 90%. Slabs shall be minimally reinforced with #4 bars placed at 16 inches on-center, positioned mid-height in the slab. Additional reinforcement requirements and an increase in thickness of the slabs-on-grade may be necessary based upon proposed loading conditions in the structures. Such loadings should be submitted to the structural and soils engineers for review.

Concrete slabs-on-grade may delete steel reinforcement provided concrete is a minimum of 7 inches in thickness. This recommendation is applicable for interior floor slab areas and exterior concrete pavement.

A vapor barrier should be utilized in areas which would be sensitive to the infiltration of moisture. This membrane should be placed within a 4 inch thick sand layer and not directly beneath the slab. Subgrade soils shall be moistened to approximately 130% of optimum levels to a depth of 18 inches as verified by the soils engineer immediately prior to pouring of concrete. All concrete slab areas to receive floor coverings should be moisture tested to meet all manufacturer requirements prior to placement.

Utility Trench Backfill

Fill soils placed were compacted to a minimum of 90% of the laboratory standard in lifts not in excess of eight inches in thickness. The on-site soils were utilized as backfill material with maximum depths consisting of the following:

| | Depth (ft) |
|--|--|
| Sewer Vapor Extraction Storm Drain Fire Service Electrical | 9' 4' (slurry capped with 1' fill) 5' 3' 31/2' |
| Water | 2' |

It should be noted that the observation of backfill material (shading) placed within the "pipe zone" was not within the scope of our services. Compaction of the utility backfill soils was achieved by use of a backhoe mounted sheepsfoot wheel and hand operated compaction equipment. A water hose provided moisture control. A summary of compaction test results is provided in Appendix B and locations of these tests are shown on the attached plan.

Wall Backfill Operations

Construction of the retaining wall located along the north end of the site is under a separate City of Los Angeles Permit. A summary of the backfill operations in this area is provided in a separate compaction report (see report dated October 27, 2005, Project Number 11233-04A). The wall backfill test locations and results are also included with this report.

Pavement Subgrade

The pavement subgrade areas were fine graded and compacted to a minimum of 90% of the laboratory standard. The base section consisted of crushed miscellaneous base material tested to a minimum of 95% relative compaction. The maximum depth of base material placed was approximately twelve inches. Five and ten ton steel drum rollers were utilized for compaction control and a water truck provided moisture control. A summary of compaction tests of the fine grading operations are provided in Appendix B with locations shown on the accompanying plan. Our services did not include any surveying of pavement subgrade areas prior to placement of base materials and pavement.

Corrosion Design Criteria

Representative samples of the surficial soils, typical of the subgrade soils expected to be encountered within foundation excavations, revealed negligible sulfate concentrations. Therefore, all concrete in contact with on site soils shall be designed in accordance with Table 19A-A-4 of the Uniform Building Code. Sulfate test results may be found on the attached Table III.

Expansive Soil

Due to the expansive nature of the on site soils, special attention should be given to the project design and maintenance. The attached *Expansive Soil Guidelines* should be reviewed by the engineers, architects, owner, maintenance personnel and other interested parties and considered during the design of the project and future property maintenance.

Limitations

It should be noted that our work does not warrant or guarantee that the contractor responsible for each phase of the project has performed his work in accordance with the project specifications.

We appreciate this opportunity to be of service to you. If you have any further questions, please do not hesitate to contact the undersigned.

Respectfully submitted, ROFESSION NORCAL ENGINEERING

Keith D. Tucker Project Engineer R.G.E. 841 Walter K. Mott Project Manager

Wack Mar

NorCal Engineering

Soils and Geotechnical Consultants 10641 Humbolt Street Los Alamitos, CA 90720 (562)799-9469 FAX (562)799-9459

CITY OF LOS ANGELES DEPARTMENT OF BUILDING AND SAFETY ENGINEER'S CERTIFICATE OF COMPLIANCE FOR COMPACTED EARTH FILLS

JOB ADDRESS: 1451 West Knox Street, Los Angeles

PERMIT NO.: 04030-10000-02507

LEGAL DESCRIPTION: Tract 52172, Lot 8

SOIL TESTING AGENCY: NorCal Engineering

PROPERTY OWNER'S NAME: Boeing Realty Corp

OWNER'S ADDRESS: 15480 Laguna Canyon Road #200, Irvine 92618

PER REPORTS ON OUR PROJECT NUMBER: 11233-04

DATE OF WORK STARTED ON PROJECT: 1/17/05

DATE FILL WAS COMPLETED: 9/13/05

DATE OF THIS CERTIFICATE: 10/27/05

TO THE SUPERINTENDENT OF BUILDING:

I hereby certify that I have personally inspected and tested the placing of compacted earth fill on the above described property, and on the basis of these inspections and tests it is my opinion that the same was placed in conformity with the requirements of the Los Angeles City Building Code.

Keith D. Tucker R.G.E. 841

*For the purpose of this certificate, to have "personally inspected and tested" shall include inspection and testing performed by any person responsible to the licensed engineer signing this certificate. Where the inspection and testing of all or part of the work above is delegated, full responsibility shall be assumed by the licensed engineer whose signature is affixed thereon.

Expansive Soil Guidelines

The following expansive soil guidelines are provided for your project. The intent of these guidelines is to inform you, the client, of the importance of proper design and maintenance of projects supported on expansive soils. You, as the owner or other interested party, should be warned that you have a duty to provide the information contained in the soil report including these guidelines to your design engineers, architects, landscapers and other design parties in order to enable them to provide a design that takes into consideration expansive soils.

In addition, you should provide the soil report with these guidelines to any property manager, lessee, property purchaser or other interested party that will have or assume the responsibility of maintaining the development in the future.

Expansive soils are fine-grained silts and clays which are subject to swelling and contracting. The amount of this swelling and contracting is subject to the amount of fine-grained clay materials present in the soils and the amount of moisture either introduced or extracted from the soils. Expansive soils are divided into five categories ranging from "very low" to "very high". Expansion indices are assigned to each classification and are included in the laboratory testing section of this report. If the expansion index of the soils on your site, as stated in this report, is 21 or higher, you have expansive soils. The classifications of expansive soils are as follows:

Classification of Expansive Soil*

| Expansion Index | Potential Expansion |
|-----------------|---------------------|
| 0-20 | Very Low |
| 21-50 | Low |
| 51-90 | Medium |
| 91-130 | High |
| Above 130 | Very High |

^{*}From Table 18A-I-B of California Building Code (1988)

When expansive soils are compacted during site grading operations, care is taken to place the materials at or slightly above optimum moisture levels and perform proper compaction operations. Any subsequent excessive wetting and/or drying of expansive soils will cause the soil materials to expand and/or contract. These actions are likely to cause distress of foundations, structures, slabs-on-grade, sidewalks and pavement over the life of the structure. It is therefore imperative that even after construction of improvements, the moisture contents are maintained at relatively constant levels, allowing neither excessive wetting or drying of soils.

Evidence of excessive wetting of expansive soils may be seen in concrete slabs, both interior and exterior. Slabs may lift at construction joints producing a trip hazard or may crack from the pressure of soil expansion. Wet clays in foundation areas may result in lifting of the structure causing difficulty in the opening and closing of doors and windows, as well as cracking in exterior and interior wall surfaces. In extreme wetting of soils to depth, settlement of the structure may eventually result. Excessive wetting of soils in landscape areas adjacent to concrete or asphaltic pavement areas may also result in expansion of soils beneath pavement and resultant distress to the pavement surface.

Excessive drying of expansive soils is initially evidenced by cracking in the surface of the soils due to contraction. Settlement of structures and on-grade slabs may also eventually result along with problems in the operation of doors and windows.

Projects located in areas of expansive clay soils will be subject to more movement and "hairline" cracking of walls and slabs than similar projects situated on non-expansive sandy soils. There are, however, measures that developers and property owners may take to reduce the amount of movement over the life the development. The following guidelines are provided to assist you in both design and maintenance of projects on expansive soils:

- Drainage away from structures and pavement is essential to prevent excessive wetting of expansive soils. Grades of at least 3% should be designed and maintained to allow flow of irrigation and rain water to approved drainage devices or to the street. Any "ponding" of water adjacent to buildings, slabs and pavement after rains is evidence of poor drainage; the installation of drainage devices or regrading of the area may be required to assure proper drainage. Installation of rain gutters is also recommended to control the introduction of moisture next to buildings. Gutters should discharge into a drainage device or onto pavement which drains to roadways.
- Irrigation should be strictly controlled around building foundations, slabs and
 pavement and may need to be adjusted depending upon season. This
 control is essential to maintain a relatively uniform moisture content in the
 expansive soils and to prevent swelling and contracting. Over-watering
 adjacent to improvements may result in damage to those improvements.
 NorCal Engineering makes no specific recommendations regarding
 landscape irrigation schedules.
- Planting schemes for landscaping around structures and pavement should be analyzed carefully. Plants (including sod) requiring high amounts of water may result in excessive wetting of soils. Trees and large shrubs may actually extract moisture from the expansive soils, thus causing contraction of the fine-grained soils.

- Thickened edges on exterior slabs will assist in keeping excessive moisture from entering directly beneath the concrete. A six-inch thick or greater deepened edge on slabs may be considered. Underlying interior and exterior slabs with 6 to 12 inches or more of non-expansive soils and providing presaturation of the underlying clayey soils as recommended in the soil report will improve the overall performance of on-grade slabs.
- Increase the amount of steel reinforcing in concrete slabs, foundations and other structures to resist the forces of expansive soils. The precise amount of reinforcing should be determined by the appropriate design engineers and/or architects.
- Recommendations of the soil report should always be followed in the development of the project. Any recommendations regarding presaturation of the upper subgrade soils in slab areas should be performed in the field and verified by the Soil Engineer.

APPENDICES (In order of appearance)

Appendix A – Laboratory Tests

Table I – Maximum Density Tests
Table II – Expansion Index Tests
Table III – Sulfate Tests

Plate A - Direct Shear Tests

Appendix B - Summary of Compaction Tests

Site Plan
Summary of Compaction Tests

Appendix C - City of Los Angeles Approval Letters

Appendix A

TABLE I MAXIMUM DENSITY TESTS (ASTM: D1557-00)

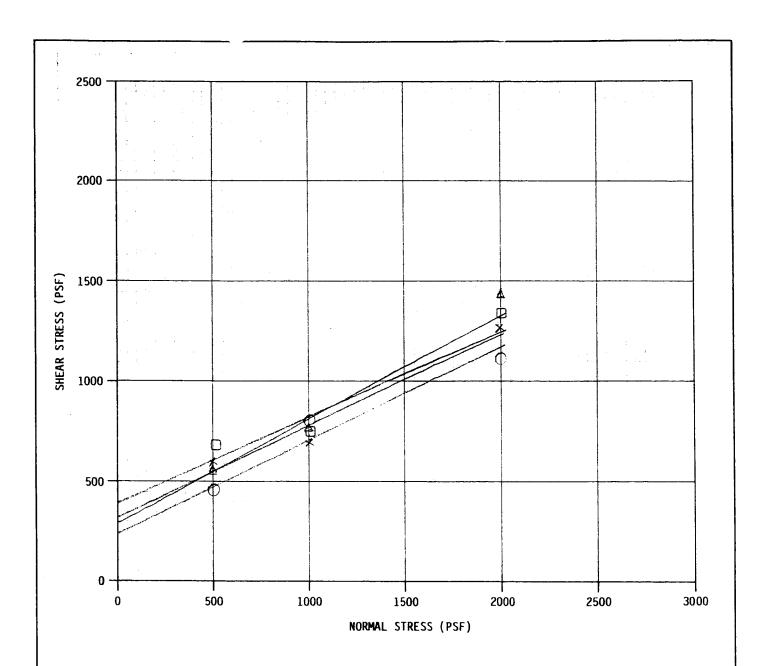
| <u>Sample</u> | Classification | Optimum <u>Moisture</u> | Maximum Dry Density (lbs./cu.ft.) |
|---------------|------------------------------------|----------------------------|--------------------------------------|
| i | Silty sandy CLAY | 13.5 | 124.0 |
| II | Silty sandy CLAY | 12.5 | 126.0 |
| 111 | Silty sandy CLAY | 12.0 | 125.5 |
| IV | Silty sandy CLAY | 10.0 | 126.5 |
| ٧ | SAND fine to coarse grained, silty | 8.5 | 127.0 |
| VI | Silty sandy CLAY | 13.5 | 122.0 |
| VII | Crushed Miscellaneous Base | 8.0 | 125.0 |
| VIII | Crushed Miscellaneous Base | 9.0 | 130.0 |

TABLE II EXPANSION INDEX TESTS (U.B.C. STD. 18-2)

| Sample | Classification | Expansion <u>Index</u> |
|--------------|------------------|---------------------------|
| Pad Subgrade | Silty sandy CLAY | 51 |

TABLE III SULFATE TESTS (CA. TEST METHOD 417)

| <u>Sample</u> | Sulfate (% by Weight) |
|--|-------------------------|
| Pad Subgrade Pad Subgrade Pad Subgrade | 0.016 0.020 0.011 |
| • | |



| SYMBOL | BORING NUMBER | DEPTH (FEET) | ø (DEGREES) | C (PSF) | DRY DENSITY (PCF) | MOISTURE CONTENT (%) |
|--------|------------------|-----------------|----------------|------------|-------------------------|----------------------------|
| X | T-1 | 3.0 | 25 | 325 | 112.9 | 14 9 |
| 0 | T-1 | 5.0 | 25 | 250 | 110.2 | 9.7 |
| Δ | T-3 | 7.0 | 27 | 300 | 117.3 | 10.7 |
| | T-4 | 10.0 | 23. | 400 | 110.8 | 14.6 |

NOTE: TESTS PERFORMED ON SATURATED SAMPLES UNLESS SHOWN BELOW.

(FM) FIELD MOISTURE

TESTS PERFORMED ON UNDISTURBED SAMPLES UNLESS SHOWN BELOW.

(R) SAMPLES REMOLDED AT 90% OF MAXIMUM DRY DENSITY

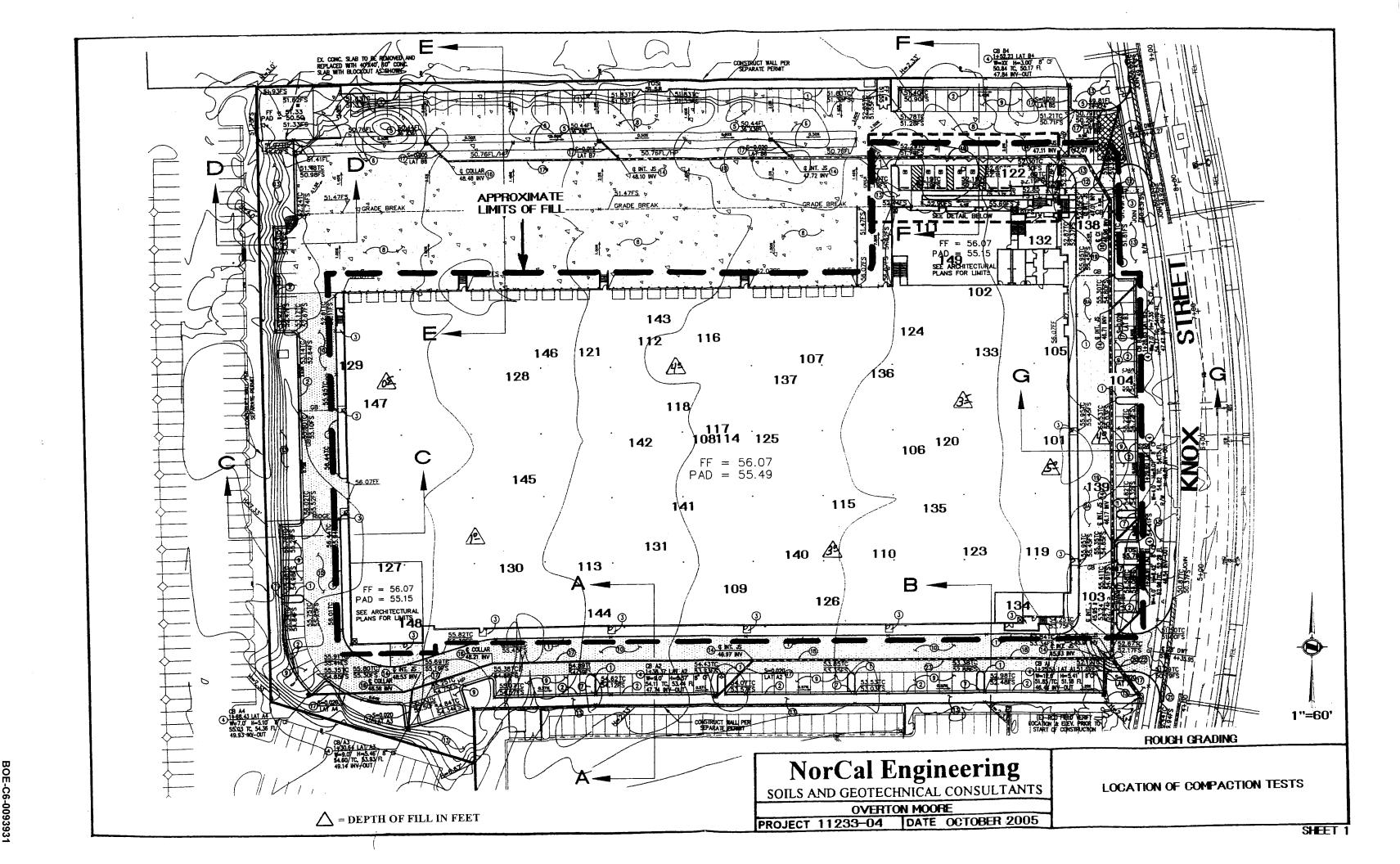
NorCal Engineering SOILS AND GEOTECHNICAL CONSULTANTS

PLATE A

DIRECT SHEAR TEST RESULTS

PROJECT 11233-04 DATE MARCH 2004

Appendix B



BOE-C6-009

CONSTRUCTION SET

Athtin none

| Date of <u>Test</u> | Test <u>No.</u> | Location | <u>Depth</u> | Percent <u>Moisture</u> | Unit Wt. lbs./cu.ft. | Relative Compaction | Soil <u>Type</u> | Test <u>S/D</u> |
|--|-----------------------------|--|--|------------------------------|----------------------------------|------------------------|---------------------|----------------------|
| 1/17/05 1/17/05 1/17/05 1/17/05 | 101 102 103 104 | Site Grading Site Grading Site Grading Site Grading | 5.0-5.5 3.0-3.5 3.0-3.5 4.0-4.5 | 14.1 12.5 14.4 15.4 | 112.1 117.3 114.5 112.7 | 90 93 92 91 | } | S S S S |
| 1/17/05 1/17/05 1/18/05 1/18/05 | 105 106 107 108 | Site Grading Site Grading Site Grading Site Grading | 4.0-4.5 3.5-4.0 3.0-3.5 2.0-2.5 | 13.8 11.3 14.0 16.5 | 119.9 122.2 117.5 108.1 | 95 97 95 87 | 11 11 1 | S S S S |
| 1/18/05 1/18/05 1/18/05 1/18/05 | 108A** 109 110 111 | Site Grading Site Grading Site Grading Site Grading | 5.0-5.5 2.0-2.5 2.0-2.5 2.0-2.5 | 13.7 13.1 13.3 13.9 | 114.3 117.5 115.6 117.6 | 92 93 92 95 | [| \$ \$ \$ \$ |
| 1/18/05 1/18/05 1/18/05 1/18/05 | 112 113 114 115 | Site Grading Site Grading Site Grading Site Grading | 4.0-4.5 1.0-1.5 3.0-3.5 1.5-2.0 | 12.4 12.6 14.1 12.0 | 118.2 120.7 113.9 116.0 | 94 96 92 92 | { | S S S S |
| 1/18/05 1/18/05 1/18/05 1/18/05 | 116 117 118 119 | Site Grading Site Grading Site Grading Site Grading | 2.0-2.5 2.0-2.5 3.0-3.5 2.0-2.5 | 12.8 12.6 13.7 13.5 | 112.5 113.6 117.2 112.7 | 91 92 93 91 | - | S S S |
| 1/18/05 1/18/05 1/19/05 1/19/05 | 120 121 122 122A** | Site Grading Site Grading Site Grading Site Grading | 2.0-2.5 1.5-2.0 1.0-1.5 1.0-1.5 | 12.5 13.0 13.1 13.0 | 114.6 118.5 115.8 119.3 | 92 94 92 95 | | \$ \$ \$ \$ |
| 1/19/05 1/19/05 1/19/05 1/19/05 | 123 124 125 126 | Site Grading Site Grading Site Grading Site Grading | 1.0-1.5 1.0-1.5 1.0-1.5 0.5-1.0 | 12.9 12.0 13.6 13.3 | 120.5 121.4 117.9 120.0 | 96 96 95 97 | | \$ \$ \$ \$ |
| 1/19/05 1/19/05 1/19/05 1/19/05 | 127 128 129 130 | Site Grading Site Grading Site Grading Site Grading | 0.5-1.0 1.0-1.5 0.5-1.0 1.0-1.5 | 12.7 13.3 12.4 12.6 | 122.4 118.2 120.9 120.6 | 97 95 96 96 | | S S S |

**Retest of failing tests after area reworked S= Sand Cone Method

| Date of <u>Test</u> | Test <u>No.</u> | <u>Location</u> | <u>Depth</u> | Percent <u>Moisture</u> | Unit Wt. lbs./cu.ft. | Relative Compaction | Soil <u>Type</u> | Test <u>S/D</u> |
|--|-----------------------------|--|--|------------------------------|----------------------------------|------------------------|----------------------|--------------------|
| 1/19/05 | 131 | Site Grading | 1.5-2.0 | 12.6 | 119.8 | 97 | | \$ |
| 1/20/05 | 132 | Site Grading | 0.5-1.0 | 12.3 | 122.8 | 97 | | \$ |
| 1/20/05 | 133 | Site Grading | 0.0-0.5 | 12.9 | 117.8 | 95 | | \$ |
| 1/20/05 | 134 | Site Grading | 0.0-0.5 | 13.5 | 118.9 | 96 | | \$ |
| 1/20/05 | 135 | Site Grading | 0.0-0.5 | 13.0 | 120.3 | 95 | † | S |
| 1/20/05 | 136 | Site Grading | 0.0-0.5 | 13.7 | 120.4 | 97 | | S |
| 1/21/05 | 137 | Site Grading | 0.0-0.5 | 12.7 | 120.6 | 96 | } | S |
| 1/21/05 | 138 | Site Grading | 2.0-2.5 | 13.2 | 117.4 | 93 | } | S |
| 1/21/05 | 139 | Site Grading | 1.0-1.5 | 12.6 | 119.8 | 95 | | S |
| 1/21/05 | 140 | Site Grading | 0.0-0.5 | 12.5 | 121.7 | 97 | | S |
| 1/21/05 | 141 | Site Grading | 0.0-0.5 | 12.7 | 118.8 | 96 | | S |
| 1/21/05 | 142 | Site Grading | 0.0-0.5 | 12.9 | 119.5 | 96 | | S |
| 1/22/05 1/22/05 1/22/05 1/22/05 | 143 144 145 146 | Site Grading Site Grading Site Grading Site Grading | 0.0-0.5 0.0-0.5 0.0-0.5 0.0-0.5 | 12.6 13.4 12.5 12.8 | 118.1 119.0 120.5 122.3 | 95 96 96 97 | | S S S S |
| 1/22/05 1/22/05 1/22/05 1/22/05 | 147 147A** 148 149 | Site Grading Site Grading Site Grading Site Grading | 0.0-0.5 0.0-0.5 0.0-0.5 0.0-0.5 | 13.1 13.1 12.6 12.9 | 116.7 118.1 119.0 121.3 | 94 95 96 96 | ! | S S S S |
| 1/24/05 | 150 | Site Grading | 1.0-1.5 | 12.6 | 118.1 | 95 | | S |
| 1/24/05 | 151 | Site Grading | 1.5-2.0 | 13.3 | 115.5 | 93 | | S |
| 1/24/05 | 152 | Site Grading | 1.0-1.5 | 13.5 | 118.9 | 96 | | S |
| 1/24/05 | 153 | Site Grading | 1.5-2.0 | 12.8 | 117.0 | 94 | | S |
| 1/24/05 | 154 | Site Grading | 0.5-1.0 | 13.1 | 119.3 | 96 | | S |
| 1/24/05 | 155 | Site Grading | 0.5-1.0 | 10.0 | 121.4 | 97 | | S |
| 1/25/05 | 156 | Ramp Subgrade | 0.0-0.5 | 13.6 | 117.9 | 95 | | S |
| 1/25/05 | 157 | Sewer | 0.0-0.5 | 12.3 | 119.5 | 96 | | S |
| 2/3/05 | 158 | Sewer | 6.0-6.5 | 12.1 | 117.5 | 93 | | \$ |
| 2/3/05 | 159 | Sewer | 4.0-4.5 | 11.6 | 116.5 | 92 | V | \$ |
| 2/3/05 | 160 | Sewer | 2.0-2.5 | 12.1 | 112.6 | 91 | | \$ |
| 2/3/05 | 161 | Sewer | 1.0-1.5 | 10.5 | 117.3 | 93 | | \$ |

**Retest of failing tests after area reworked S= Sand Cone Method

| Date of <u>Test</u> | Test <u>No.</u> | <u>Location</u> | <u>Depth</u> | Percent <u>Moisture</u> | Unit Wt. lbs./cu.ft. | Relative Compaction | Soil <u>Type</u> | Test <u>S/D</u> |
|--|-----------------------------|--|--|------------------------------|----------------------------------|------------------------|----------------------|----------------------|
| 2/3/05 2/4/05 2/4/05 2/4/05 | 162 163 164 165 | Sewer Sewer Sewer Sewer | 0.0-0.5 0.0-0.5 0.0-0.5 3.0-3.5 | 10.9 13.6 9.2 10.8 | 120.8 121.9 120.2 116.9 | 96 97 95 93 | V | S S S S |
| 2/4/05 2/4/05 2/4/05 2/4/05 | 166 167 168 169 | Sewer Sewer Sewer Sewer | 1.0-1.5 5.0-5.5 3.0-3.5 1.0-1.5 | 11.2 13.4 11.8 12.2 | 115.0 117.2 115.3 115.6 | 91 93 93 92 | IV | S S S |
| 2/4/05 2/4/05 2/4/05 2/7/05 | 170 171 172 173 | Sewer Sewer Sewer Sewer | 7.0-7.5 5.0-5.5 3.0-3.5 2.0-2.5 | 14.2 13.6 12.8 10.5 | 114.7 117.4 117.0 115.3 | 91 93 93 91 | V | S S S |
| 2/7/05 2/7/05 2/7/05 2/7/05 | 174 175 176 177 | Sewer Sewer Sewer Sewer | 1.0-1.5 0.0-0.5 0.0-0.5 2.0-2.5 | 12.1 13.0 12.5 10.9 | 114.2 120.7 120.0 115.4 | 92 96 95 92 | i II II III | \$ \$ \$ \$ |
| 2/7/05 2/7/05 2/10/05 2/10/05 | 178 179 180 181 | Sewer Sewer Vapor Extraction Vapor Extraction | 0.0-0.5 0.0-0.5 0.0-0.5 0.0-0.5 | 11.7 8.8 11.8 11.5 | 118.2 121.0 122.6 121.1 | 95 95 97 96 | | \$ \$ \$ \$ |
| 2/10/05 2/10/05 2/10/05 2/10/05 | 182 183 184 184A** | Vapor Extraction Vapor Extraction Vapor Extraction Vapor Extraction | 0.0-0.5 0.5-1.0 0.0-0.5 0.0-0.5 | 12.1 12.7 12.3 12.5 | 119.5 120.1 114.3 120.0 | 96 95 92 97 | | S S S |
| 2/10/05 2/10/05 2/15/05 2/15/05 | 185 186 187 188 | Storm Drain Storm Drain Storm Drain Storm Drain | 3.0-3.5 1.0-1.5 2.0-2.5 1.0-1.5 | 13.1 12.5 14.1 13.3 | 114.9 115.6 113.9 112.9 | 91 93 92 91 | - - - - | S S S S |
| 2/17/05 2/17/05 3/7/05 3/7/05 | 189 190 191 192 | Storm Drain Storm Drain Vapor Extraction Vapor Extraction | 2.5-3.0 1.0-1.5 0.0-0.5 0.0-0.5 | 12.5 13.1 14.4 7.9 | 116.2 114.9 120.4 108.1 | 92 93 96 87 | - | S S S |

**Retest of failing tests after area reworked S= Sand Cone Method

| Date of <u>Test</u> | Test <u>No.</u> | <u>Location</u> | <u>Depth</u> | Percent <u>Moisture</u> | Unit Wt. lbs./cu.ft. | Relative Compaction | Soil Type | Test <u>S/D</u> |
|--------------------------------------|--------------------------|--|--|------------------------------|----------------------------------|------------------------|-----------------------|--------------------|
| 3/21/05 | 192A** | Vapor Extraction | 0.0-0.5 | 11.6 | 118.7 | 96 | | S |
| 3/21/05 | 193 | Vapor Extraction | 0.0-0.5 | 12.1 | 121.1 | 96 | | S |
| 3/21/05 | 194 | Vapor Extraction | 0.0-0.5 | 12.8 | 119.9 | 95 | | S |
| 3/22/05 | 195 | Vapor Extraction | 0.0-0.5 | 12.7 | 120.2 | 95 | | S |
| 3/22/05 | 196 | Vapor Extraction | 0.0-0.5 | 13.3 | 121.0 | 96 | | S |
| 4/5/05 | 197 | Vapor Extraction | 0.0-0.5 | 13.9 | 122.1 | 97 | | S |
| 4/5/05 | 198 | Vapor Extraction | 0.0-0.5 | 12.9 | 120.4 | 96 | | S |
| 4/5/05 | 199 | Vapor Extraction | 0.0-0.5 | 12.1 | 118.6 | 96 | | S |
| 4/5/05 | 200 | Sewer | 6.0-6.5 | 11.9 | 114.3 | 92 | | \$ |
| 4/5/05 | 201 | Sewer | 4.0-4.5 | 12.8 | 116.8 | 93 | - | \$ |
| 4/5/05 | 202 | Sewer | 2.0-2.5 | 11.0 | 114.8 | 91 | - | \$ |
| 4/5/05 | 203 | Sewer | 3.0-3.5 | 12.1 | 114.2 | 92 | - | \$ |
| 4/5/05 | 204 | Sewer Vapor Extraction Sewer Vapor Extraction | 5.0-5.5 | 13.3 | 114.7 | 93 | 1 | \$ |
| 4/5/05 | 205 | | 0.0-0.5 | 11.6 | 120.9 | 96 | | \$ |
| 4/5/05 | 206 | | 3.0-3.5 | 11.8 | 116.5 | 92 | V | \$ |
| 4/6/05 | 207 | | 0.0-0.5 | 12.3 | 117.9 | 95 | | \$ |
| 4/6/05 4/6/05 4/6/05 4/6/05 | 208 209 210 211 | Vapor Extraction Fndn. Bottom Fndn. Bottom Fndn. Bottom | 0.0-0.5 8.0-8.5 7.0-7.5 6.0-6.5 | 13.3 13.0 13.8 11.9 | 119.2 115.0 111.6 117.2 | 96 91 91 93 | | S S S |
| 4/6/05 4/6/05 4/6/05 4/6/05 | 212 213 214 215 | Fndn. Bottom Fndn. Bottom Vapor Extraction Vapor Extraction | 5.0-5.5 5.0-5.5 0.0-0.5 0.0-0.5 | 13.4 10.5 11.9 13.5 | 111.1 116.7 119.2 117.9 | 91 92 96 95 | VI IV I | s s s |
| 4/6/05 | 216 | Vapor Extraction | 0.0-0.5 | 12.9 | 122.4 | 97 | | \$ |
| 4/6/05 | 217 | Sewer | 5.0-5.5 | 12.2 | 114.3 | 91 | | \$ |
| 4/6/05 | 218 | Sewer | 3.0-3.5 | 12.3 | 115.0 | 93 | | \$ |
| 4/6/05 | 219 | Sewer | 1.0-1.5 | 12.6 | 114.2 | 92 | | \$ |
| 4/13/05 | 220 | Storm Drain | 2.0-2.5 | 13.1 | 114.9 | 91 | | S |
| 4/13/05 | 221 | Storm Drain | 0.5-1.0 | 12.7 | 121.3 | 96 | | S |
| 4/13/05 | 222 | Storm Drain | 0.5-1.0 | 12.9 | 115.1 | 91 | | S |
| 4/13/05 | 223 | Storm Drain | 2.0-2.5 | 13.4 | 115.6 | 93 | | S |

**Retest of failing tests after area reworked S= Sand Cone Method

| Date of <u>Test</u> | Test <u>No.</u> | <u>Location</u> | <u>Depth</u> | Percent <u>Moisture</u> | Unit Wt. lbs./cu.ft. | Relative Compaction | Soil <u>Type</u> | Test <u>S/D</u> |
|--|--------------------------|--|--|------------------------------|----------------------------------|------------------------|---------------------|----------------------|
| 4/13/05 | 224 | Storm Drain | 0.5-1.0 | 12.5 | 1200 | 95 | | S |
| 4/13/05 | 225 | Storm Drain | 1.0-1.5 | 12.2 | 116.2 | 92 | | S |
| 4/13/05 | 226 | Storm Drain | 2.0-2.5 | 11.7 | 117.3 | 93 | | S |
| 4/14/05 | 227 | Water | 0.5-1.0 | 12.7 | 112.7 | 91 | | S |
| 4/14/05 | 228 | Water | 0.5-1.0 | 11.9 | 116.2 | 92 | | \$ |
| 4/14/05 | 229 | Storm Drain | 2.0-2.5 | 13.3 | 112.1 | 90 | | \$ |
| 4/14/05 | 230 | Storm Drain | 0.5-1.0 | 12.3 | 114.9 | 93 | | \$ |
| 4/14/05 | 231 | Storm Drain | 0.5-1.0 | 10.9 | 115.5 | 92 | | \$ |
| 4/14/05 4/14/05 4/14/05 4/14/05 | 232 233 234 235 | Storm Drain Storm Drain Storm Drain Storm Drain | 1.0-1.5 2.0-2.5 0.5-1.0 0.5-1.0 | 12.9 13.8 13.0 13.4 | 115.1 116.9 115.0 113.8 | 91 93 91 92 | | \$ \$ \$ \$ |
| 4/15/05 | 236 | Storm Drain | 2.5-3.0 | 12.4 | 113.9 | 92 | | \$ |
| 4/15/05 | 237 | Storm Drain | 0.5-1.0 | 11.6 | 116.5 | 92 | | \$ |
| 4/15/05 | 238 | Storm Drain | 2.0-2.5 | 13.3 | 113.0 | 91 | | \$ |
| 4/15/05 | 239 | Storm Drain | 1.5-2.0 | 12.2 | 113.6 | 90 | | \$ |
| 4/16/05 | 240 | Storm Drain | 3.0-3.5 | 10.9 | 117.2 | 93 | IV | S |
| 4/16/05 | 241 | Storm Drain | 1.0-1.5 | 11.1 | 116.1 | 92 | III | S |
| 4/16/05 | 242 | Storm Drain | 4.0-4.5 | 10.5 | 115.3 | 91 | IV | S |
| 4/16/05 | 243 | Storm Drain | 2.0-2.5 | 10.8 | 117.3 | 93 | IV | S |
| 4/16/05 | 244 | Storm Drain | 2.0-2.5 | 10.3 | 114.4 | 91 | | S |
| 4/16/05 | 245 | Storm Drain | 3.0-3.5 | 10.6 | 115.1 | 92 | | S |
| 4/16/05 | 246 | Storm Drain | 2.0-2.5 | 11.0 | 113.9 | 90 | V | S |
| 4/16/05 | 247 | Storm Drain | 1.0-1.5 | 10.6 | 116.6 | 93 | | S |
| 4/16/05 | 248 | Storm Drain | 2.0-2.5 | 10.2 | 115.0 | 91 | i∨ | S |
| 4/16/05 | 249 | Storm Drain | 0.0-0.5 | 10.4 | 116.6 | 93 | | S |
| 4/16/05 | 250 | Storm Drain | 0.0-0.5 | 10.8 | 115.4 | 92 | | S |
| 4/20/05 | 251 | Fire Service | 2.0-2.5 | 15.0 | 107.6 | 87 | | S |
| 4/20/05 | 251A** | Fire Service | 2.0-2.5 | 13.8 | 115.5 | 93 | | S |
| 4/20/05 | 252 | Fire Service | 2.0-2.5 | 11.7 | 116.3 | 92 | | S |
| 4/21/05 | 253 | Fire Service | 1.0-1.5 | 12.1 | 114.2 | 91 | | S |
| 4/21/05 | 254 | Fire Service | 1.5-2.0 | 13.9 | 115.7 | 92 | | S |

**Retest of failing tests after area reworked S= Sand Cone Method

| Date of | Test | | | Percent | Unit Wt. | Relative | Soil | Test |
|-------------|------------|-----------------|--------------|-----------------|-------------|------------|------|------|
| <u>Test</u> | <u>No.</u> | Location | <u>Depth</u> | <u>Moisture</u> | lbs./cu.ft. | Compaction | Type | S/D |
| 4/21/05 | 255 | Fire Service | 2.0-2.5 | 12.5 | 117.3 | 93 | П | S |
| 4/21/05 | 256 | Fire Service | 1.0-1.5 | 14.5 | 113.5 | 92 | | S |
| 4/21/05 | 257 | Fire Service | 1.0-1.5 | 13.2 | 114.8 | 91 | II. | S |
| 4/21/05 | 258 | Fire Service | 2.0-2.5 | 13.5 | 115.6 | 93 | l | S |
| 4/21/05 | 259 | Fire Service | 1.0-1.5 | 14.5 | 112.7 | 91 | 1 | S |
| 4/21/05 | 260 | Fire Service | 1.0-1.5 | 13.8 | 115.1 | 93 | İ | S |
| 4/21/05 | 261 | Fire Service | 1.5-2.0 | 12.9 | 116.1 | 92 | II. | S |
| 4/21/05 | 262 | Fire Service | 1.0-1.5 | 13.2 | 113.0 | 91 | ļ | S |
| 4/21/05 | 263 | Fire Service | 1.5-2.0 | 13.6 | 117.1 | 93 | 11 | S |
| 4/21/05 | 264 | Fire Service | 1.0-1.5 | 11.2 | 115.3 | 91 | IV | S |
| 4/21/05 | 265 | Fire Service | 0.5-1.0 | 13.3 | 114.7 | 93 | I | S |
| 4/21/05 | 266 | Fire Service | 1.0-1.5 | 12.7 | 112.7 | 91 | l | S |
| 4/21/05 | 267 | Fire Service | 1.0-1.5 | 13.1 | 115.8 | 93 | 1 | S |
| 5/26/05 | 268 | Wall Backfill | 1.5-2.0 | 11.7 | 116.0 | 92 | Ш | S |
| 5/26/05 | 269 | Wall Backfill | 1.5-2.0 | 11.1 | 114.8 | 91 | IV | S |
| 5/27/05 | 270 | Wall Backfill | 1.0-1.5 | 11.5 | 115.2 | 93 | I | S |
| 5/27/05 | 271 | Wall Backfill | 1.0-1.5 | 12.8 | 114.4 | 91 | 11 | S |
| 5/27/05 | 272 | Wall Backfill | 1.0-1.5 | 11.5 | 113.9 | 90 | II | S |
| 5/27/05 | 273 | Wall Backfill | 1.5-2.0 | 12.9 | 108.1 | 86 | II | S |
| 5/27/05 | 273A** | Wall Backfill | 1.5-2.0 | 12.4 | 113.8 | 90 | H | S |
| 5/27/05 | 274 | Wall Backfill | 1.5-2.0 | 13.8 | 114.2 | 92 | ŀ | S |
| 5/27/05 | 275 | Wall Backfill | 1.0-1.5 | 10.3 | 108.1 | 86 | Ш | S |
| 5/27/05 | 275A** | Wall Backfill | 1.0-1.5 | 10.9 | 115.5 | 92 | Ш | S |
| 5/27/05 | 276 | Wall Backfill | 0.0-0.5 | 10.1 | 120.2 | 95 | IV | S |
| 5/31/05 | 277 | Wall Backfill | 1.0-1.5 | 13.7 | 115.6 | 92 | П | S |
| 5/31/05 | 278 | Wall Backfill | 1.0-1.5 | 13.3 | 113.8 | 91 | 11 | S |
| 5/31/05 | 279 | Wall Backfill | 0.0-0.5 | 13.5 | 116.8 | 93 | 11 | S |
| 5/31/05 | 280 | Wall Backfill | 0.0-0.5 | 14.1 | 118.0 | 95 | ı | S |
| 5/31/05 | 281 | Wall Backfill | 0.0-0.5 | 10.5 | 120.4 | 95 | IV | S |
| 6/8/05 | 282 | Curb/Gutter Sg. | 0.0-0.5 | 11.5 | 117.3 | 93 | | S |
| 6/8/05 | 283 | Curb/Gutter Sg. | 0.0-0.5 | 10.9 | 116.6 | 92 | ١٧ | S |
| 6/8/05 | 284 | Curb/Gutter Sg. | 0.0-0.5 | 10.3 | 116.9 | 93 | Ш | S |

**Retest of failing tests after area reworked S= Sand Cone Method

| Date of Test | Test <u>No.</u> | <u>Location</u> | <u>Depth</u> | Percent <u>Moisture</u> | Unit Wt. lbs./cu.ft. | Relative Compaction | Soil <u>Type</u> | Test <u>S/D</u> |
|--|--------------------------|---|--|------------------------------|----------------------------------|------------------------|----------------------|--------------------|
| 6/8/05 | 285 | Curb/Gutter Sg. | 0.0-0.5 | 11.3 | 114.9 | 91 | 11 | S |
| 6/9/05 | 286 | Curb/Gutter Sg. | 0.0-0.5 | 11.1 | 114.5 | 91 | 14 | S |
| 6/9/05 | 287 | Curb/Gutter Sg. | 0.0-0.5 | 10.5 | 117.6 | 93 | 1 | S |
| 6/9/05 | 288 | Curb/Gutter Sg. | 0.0-0.5 | 11.0 | 117.1 | 93 | 111 | S |
| 6/9/05 6/9/05 6/9/05 6/9/05 | 289 290 291 292 | Curb/Gutter Sg. Curb/Gutter Sg. Curb/Gutter Sg. Drive App. Sg. | 0.0-0.5 0.0-0.5 0.0-0.5 0.0-0.5 | 11.9 11.7 12.2 14.1 | 111.7 116.6 113.5 113.0 | 90 92 90 91 | I IV II I | S S S |
| 6/9/05 | 293 | Ramp Backfill | 1.0-1.5 | 10.5 | 122.4 | 96 | V | \$ |
| 6/9/05 | 294 | Ramp Subgrade | 0.0-0.5 | 13.1 | 120.2 | 95 | | \$ |
| 6/16/05 | 295 | Electrical | 1.0-1.5 | 13.6 | 115.7 | 92 | | \$ |
| 6/16/05 | 296 | Electrical | 1.0-1.5 | 11.6 | 113.8 | 90 | | \$ |
| 6/16/05 6/16/05 6/16/05 6/16/05 | 297 298 299 300 | Electrical Electrical Electrical Electrical | 1.5-2.0 0.0-0.5 0.0-0.5 0.0-0.5 | 15.0 14.2 13.9 11.2 | 114.8 113.1 114.3 116.5 | 93 91 92 93 | l | S S S |
| 6/17/05 | 301 | Stair Backfill | 2.0-2.5 | 10.5 | 114.9 | 92 | | \$ |
| 6/17/05 | 302 | Stair Backfill | 0.0-0.5 | 11.5 | 113.6 | 90 | | \$ |
| 6/20/05 | 303 | Curb/Gutter Sg. | 0.0-0.5 | 12.2 | 113.2 | 91 | | \$ |
| 6/20/05 | 304 | Curb/Gutter Sg. | 0.0-0.5 | 11.1 | 113.4 | 91 | | \$ |
| 6/20/05 | 305 | Curb/Gutter Sg. | 0.0-0.5 | 11.5 | 117.5 | 93 | | S |
| 6/20/05 | 306 | Curb/Gutter Sg. | 0.0-0.5 | 12.0 | 116.2 | 92 | | S |
| 6/20/05 | 307 | Electrical | 1.0-1.5 | 11.6 | 113.8 | 92 | | S |
| 6/20/05 | 308 | Electrical | 0.5-1.0 | 12.4 | 112.1 | 90 | | S |
| 6/24/05 | 309 | Drive App. Sg. | 0.0-0.5 | 8.2 | 120.6 | 96 | VII | S |
| 6/29/05 | 310 | Vapor Extraction | 0.0-0.5 | 16.5 | 109.3 | 87 | III | S |
| 6/29/05 | 310A** | Vapor Extraction | 0.0-0.5 | 12.7 | 116.9 | 93 | III | S |
| 6/29/05 | 311 | Vapor Extraction | 0.0-0.5 | 11.1 | 114.8 | 91 | IV | S |
| 6/29/05 | 312 | Vapor Extraction | 0.0-0.5 | 11.3 | 116.1 | 92 | IV | S |
| 6/29/05 | 313 | Vapor Extraction | 0.0-0.5 | 13.0 | 116.7 | 93 | III | S |
| 6/29/05 | 314 | Vapor Extraction | 0.0-0.5 | 11.8 | 117.7 | 93 | IV | S |
| 6/30/05 | 315 | Vapor Extraction | 0.0-0.5 | 10.6 | 114.4 | 90 | IV | S |

**Retest of failing tests after area reworked S= Sand Cone Method

| Date of <u>Test</u> | Test <u>No.</u> | <u>Location</u> | <u>Depth</u> | Percent <u>Moisture</u> | Unit Wt. lbs./cu.ft. | Relative Compaction | Soil Type | Test S/D |
|--|-----------------------------|--|--|------------------------------|----------------------------------|------------------------|------------------------|----------------------|
| 7/8/05 7/8/05 7/8/05 7/14/05 | 316 317 318 319 | Vapor Extraction Vapor Extraction Vapor Extraction Vapor Extraction | 0.0-0.5 0.0-0.5 0.0-0.5 0.0-0.5 | 9.8 10.2 11.4 10.0 | 118.4 122.0 120.5 120.9 | 95 96 95 96 | III IV IV | S S S S |
| 7/14/05 7/14/05 7/15/05 7/15/05 | 320 321 322 323 | Vapor Extraction Vapor Extraction Vapor Extraction Vapor Extraction | 0.0-0.5 0.0-0.5 0.0-0.5 0.0-0.5 | 10.8 9.8 10.3 9.9 | 120.3 119.5 120.2 120.4 | 96 95 96 95 | V | S S S S |
| 7/21/05 7/21/05 7/21/05 7/21/05 | 324 324A** 325 326 | Vapor Extraction Vapor Extraction Vapor Extraction Vapor Extraction | 0.0-0.5 0.0-0.5 0.0-0.5 0.0-0.5 | 12.9 10.8 11.1 12.5 | 109.8 120.6 122.4 120.8 | 87 96 97 96 | V | S S S |
| 7/25/05 7/25/05 7/30/05 7/30/05 | 327 328 329 330 | Vapor Extraction Vapor Extraction Storm Drain Storm Drain | 0.0-0.5 0.0-0.5 4.0-4.5 2.0-2.5 | 12.9 11.9 11.1 10.7 | 122.2 119.4 116.1 116.6 | 97 95 92 93 | V | S S S S |
| 7/30/05 7/30/05 7/30/05 7/30/05 | 331 332 333 334 | Storm Drain Storm Drain Storm Drain Storm Drain | 3.0-3.5 1.0-1.5 1.0-1.5 2.0-2.5 | 11.5 11.7 11.3 11.5 | 115.3 117.5 115.3 116.9 | 91 93 92 93 | IV IV III III | S S S S |
| 7/30/05 7/30/05 7/30/05 7/30/05 | 335 336 337 338 | Storm Drain Storm Drain Storm Drain Storm Drain | 1.5-2.0 1.0-1.5 0.0-0.5 0.0-0.5 | 10.9 11.2 10.3 10.6 | 115.3 116.5 116.0 115.7 | 91 93 92 91 | V V | S S S |
| 7/30/05 8/2/05 8/2/05 8/15/05 | 339 340 341 342 | Storm Drain Vapor Extraction Vapor Extraction Vapor Extraction | 0.0-0.5 0.0-0.5 0.0-0.5 0.0-0.5 | 10.8 11.9 11.7 11.7 | 114.6 120.4 120.7 115.3 | 91 95 95 92 | V V | \$ \$ \$ \$ |
| 8/15/05 8/15/05 8/15/05 8/16/05 | 343 344 345 346 | Vapor Extraction Vapor Extraction Vapor Extraction Vapor Extraction | 0.0-0.5 0.0-0.5 0.0-0.5 0.0-0.5 | 11.2 11.5 10.9 9.5 | 116.9 119.4 112.3 116.4 | 93 95 93 92 | V | S S S |

**Retest of failing tests after area reworked S= Sand Cone Method

| Date of <u>Test</u> | Test <u>No.</u> | <u>Location</u> | <u>Depth</u> | Percent Moisture | Unit Wt. lbs./cu.ft. | Relative Compaction | Soil <u>Type</u> | Test <u>S/D</u> |
|--|--------------------------|--|--|-----------------------------|----------------------------------|------------------------|--------------------------|----------------------|
| 8/16/05 8/16/05 8/16/05 8/16/05 | 347 348 349 350 | Vapor Extraction Vapor Extraction Vapor Extraction Electrical | 0.0-0.5 0.0-0.5 0.0-0.5 0.0-0.5 | 8.9 10.8 10.5 10.3 | 117.5 114.3 116.9 115.2 | 93 91 93 91 | IV III III IV | S S S |
| 8/16/05 8/18/05 8/18/05 8/18/05 | 351 352 353 354 | Electrical Electrical Electrical Electrical | 0.0-0.5 0.0-0.5 0.0-0.5 0.0-0.5 | 12.6 10.3 9.4 9.8 | 116.5 115.6 114.3 113.6 | 93 92 91 90 | V | \$ \$ \$ \$ |
| 8/18/05 8/18/05 8/22/05 8/22/05 | 355 356 357 358 | Electrical Electrical Vapor Extraction Vapor Extraction | 0.0-0.5 0.0-0.5 0.0-0.5 0.0-0.5 | 10.6 9.9 10.6 10.2 | 116.5 117.4 119.5 115.6 | 92 93 95 92 | IV IV III III | \$ \$ \$ \$ |
| 8/25/05 8/25/05 8/25/05 8/25/05 | 359 360 361 362 | Drive App. Sg. Drive App. Sg. Drive App. Sg. Drive App. Sg. | 0.0-0.5 0.0-0.5 0.0-0.5 0.0-0.5 | 9.3 9.9 9.6 9.3 | 116.6 116.2 115.2 115.6 | 93 92 91 92 | V V | \$ \$ \$ \$ |
| 8/25/05 8/25/05 8/26/05 8/26/05 | 363 364 365 366 | Drive App. Sg. Drive App. Sg. Curb/Gutter Sg. Curb/Gutter Sg. | 0.0-0.5 0.0-0.5 0.0-0.5 0.0-0.5 | 9.1 9.2 9.8 10.9 | 114.1 116.5 115.8 115.3 | 91 93 92 92 | V | S S S |
| 8/26/05 8/26/05 8/26/05 8/26/05 | 367 368 369 370 | Curb/Gutter Sg. Curb/Gutter Sg. Curb/Gutter Sg. Curb/Gutter Sg. | 0.0-0.5 0.0-0.5 0.0-0.5 0.0-0.5 | 10.4 9.5 9.2 9.8 | 117.6 114.2 115.6 114.0 | 93 90 92 91 | IV IV III | S S S S |
| 8/26/05 8/26/05 8/31/05 8/31/05 | 371 372 373 374 | Curb/Gutter Sg. Curb/Gutter Sg. Curb/Gutter Base Curb/Gutter Base | 0.0-0.5 0.0-0.5 0.0-0.5 0.0-0.5 | 10.5 9.9 8.3 7.8 | 117.8 116.4 125.8 126.2 | 93 92 97 97 | IV IV VIII VIII | S S S |
| 9/1/05 9/1/05 9/1/05 9/1/05 | 375 376 377 378 | Parking Subgrade Parking Subgrade Parking Subgrade Parking Subgrade | 0.0-0.5 0.0-0.5 | 10.9 9.2 10.0 10.5 | 117.8 115.4 118.2 115.3 | 93 91 93 92 | IV IV IV III | \$ \$ \$ \$ |

**Retest of failing tests after area reworked S= Sand Cone Method

| Date of <u>Test</u> | Test <u>No.</u> | Location | <u>Depth</u> | Percent <u>Moisture</u> | Unit Wt. lbs./cu.ft. | Relative Compaction | Soil <u>Type</u> | Test <u>S/D</u> |
|--|--------------------------|---|--|----------------------------|----------------------------------|------------------------|-----------------------|--------------------|
| 9/7/05 9/7/05 9/7/05 9/7/05 | 379 380 381 382 | Parking Base Parking Base Parking Base Parking Base | 0.0-0.5 0.0-0.5 0.0-0.5 0.0-0.5 | 9.8 9.9 8.6 8.9 | 124.6 126.3 124.6 125.8 | 96 97 96 97 | VIII VIII VIII | S S S S |
| 9/7/05 9/8/05 9/8/05 9/8/05 | 383 384 385 386 | Parking Base Parking Base Parking Base Parking Base | 0.0-0.5 0.0-0.5 0.0-0.5 0.0-0.5 | 9.5 8.1 9.1 9.3 | 124.4 126.1 124.3 124.1 | 96 97 96 95 | VIII VIII VIII | S S S S |
| 9/12/05 9/12/05 9/12/05 9/13/05 | 387 388 389 390 | Site Grading Site Grading Site Grading Truck Apron Sg. | 0.5-1.0 0.5-1.0 0.5-1.0 0.0-0.5 | 11.1 8.6 9.0 8.5 | 120.3 120.1 120.6 120.4 | 95 95 96 95 | IV IV III IV | S S S |
| 9/13/05 9/13/05 9/13/05 9/13/05 | 391 392 393 394 | Truck Apron Sg. Parking Subgrade Parking Subgrade Parking Subgrade | | 9.4 8.6 11.7 9.8 | 120.6 121.5 118.8 120.4 | 95 97 96 96 | IV | S S S |
| 9/13/05 9/13/05 | 395 396 | Truck Apron Sg. Truck Apron Sg. | 0.0-0.5 0.0-0.5 | 9.4 10.2 | 120.6 122.5 | 95 97 | IV IV | S S |

**Retest of failing tests after area reworked S= Sand Cone Method

Appendix C

DEPARTMENT OF

BUILDING AND SAFETY 201 N. FIGUEROA STREET

LOS ANGELES, CA 90012

ANDREW A. ADELMAN. GENERAL MANAGER

RICHARD E. HOLGUIN EXECUTIVE OFFICER

BOARD OF BUILDING AND SAFETY COMMISSIONERS

LEE KANON ALPERT

MABEL CHANG VICE-PRESIDENT

CORINA R. ALARCON JEANETTE APPLEGATE JOYCE L. FOSTER

CITY OF LOS ANGELES

CALIFORNIA

Fax:213



RICHARD J. RIORDAN MAYOR

January 21, 2000

Boeing Realty Corporation 4060 Lakewood Blvd. Long Beach, CA 90808-1700

TRACT:

52172-02

BLOCK:

LOT

1-12. 15-20

PERMIT No.98030-10000-00170 DISTRICT MAP NO. 57B193

COMPACTION FILE 5

LOG # 28904-01

Corrected letter to change lot numbers

LOCATION: 1414 WEST 190TH STREET

SUBJECT: SECONDARY STRUCTURAL FILL

LOTS HAVING COMPACTED FILL: 1-12, 15-20

Soils Compaction Report No. 5936-96, dated October 20, 1999, prepared by NorCal Engineering. Previous report dated August 19, 1999, by Norcal Engineering.

Approval is granted for compacted fill constructed on the above lots as described in the compaction report. Approval is limited to the area shown in the report and by the following conditions:

- This fill may be used for the support of floor slabs and pavement. However, the fill is not approved for the support of structural footings.
- Planting and irrigation of cut and fill slopes in hillside areas is required per Code Section 91.7012 of the Los Angeles City Building Code.

For compacted fill to be classified as structural fill, the soil testing laboratory responsible for controlling the placement of the fill must first, certify its placement and secondly, provide the allowable vertical and lateral bearing values which the fill can safely support. Where such values exceed those permitted in Table 18.1.A of the Los Angeles City Building Code, test data and calculations, including settlement calculations, shall be submitted for review.

David Hsu

Chief of Grading Section

Negisti H Girmay

Engineering Geologist Assoc.

(213) 977-6329

Log # 28904-01

NorCal Engineering cc:

Alex Velazgez, SP District Office

H. Glimai

NOTE: Grading oversized document is attached. (Document Type 92)

BOE-C6-0093944

11233-04

CITY OF LOS ANGELES CALIFORNIA

BUILDING AND SAFETY 201 NORTH FIGUEROA STREET LOS ANGELES, CA 90012

ANDREW A. ADELMAN, P.E. GENERAL MANAGER RAYMOND CHAN EXECUTIVE OFFICER

JAMES K. HAHN MAYOR

SOILS REPORT APPROVAL LETTER

LOG # 43975 SOILS FILE - 2

July 30, 2004

BOARD OF BUILDING AND SAFETY COMMISSIONERS

WILLIAM J. ROUSE

LAN ISRAELY

EFREN R. ABRATIQUE, P.E. FRANCISCO ARRIZON

BARBARA BOUDREAUX

Overton Moore Properties 1125 West 190th Street, # 200 Gardena, Ca 90248

TRACT:

52175-02

LOT:

LOCATION: 1451 Knox Street

| CURRENT REFERENCE | REPORT | DATE(S) OF | |
|-----------------------------|--------------|------------|--------------------|
| REPORT/LETTER(S) | <u>NO</u> | DOCUMENT | PREPARED BY |
| Addendum Report | 11233-04 | 05/20/2004 | Norcal Engineering |
| Soils Report | 11233-04 | 03/13/2004 | Norcal Engineering |
| Grading Ovrszd Doc | 11233-04 | 03/13/2004 | Norcal Engineering |
| PREVIOUS REFERENCE | REPORT | DATE(S) OF | |
| REPORT/LETTER(S) | NO. | DOCUMENT | PREPARED BY |
| Compaction Report | 5936-96B | 04/07/2003 | Norcal Engineering |
| 17 | ,, | 03/08/2002 | Norcal Engineering |
| Approval for Compaction Rep | ort 39542-01 | 04/25/2004 | LADBS |

The above current referenced reports concerning the proposed construction of a slab on grade warehouse building have been reviewed by the Grading Division of the Department of Building & Safety. The site is underlain by approved compacted fill. The compacted fill was approved as a secondary fill for both 1451 Knox Street and 1411 W. North 190th Street. The location of the proposed development including the limits of fill is shown on the compaction plot plan included in the current referenced report.

The site is not located within the liquefaction zone as shown on the "Seismic Hazard Zones" map issued by the State of California, and liquefaction study is not required.

The reports are acceptable, provided the following conditions are complied with during site development:

1. The soils engineer shall review and approve the detailed plans prior to issuance of any permit. This approval shall be by signature on the plans which clearly indicates that the